

DESIGN DEVELOPMENT AND RAPID PROTOTYPING OF RUBBER COMPONENTS USING FEA

By

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- **Education**

- B.E. Mechanical Eng. L.D. College of Engineering -1998
- M.S. Mechanical Eng. Wright State University - 2001
- Polymer Eng. Course Certifications Univ. of Akron – 2002-2003
- CNC Machinist Certificate Akron Machining Institute - 2004

- **Professional Experience**

- Mechanical Testing of Engineering Materials: MTS®, Instron® and Proprietary Servo-hydraulic and Electro-mechanical Load frames.
- Performance Characterization of Elastomeric Products.
- Finite Element Analysis of Engineering Products and Components
 - Automotive (Under the hood, suspension components, tires, etc.).
 - Biomedical (Spinal, knee, and hip implants, stents etc.)
 - Aerospace (Static and dynamic analysis for honeycomb structures etc.)
- Durability Testing and Lifetime Prediction using Accelerated Test Conditions.

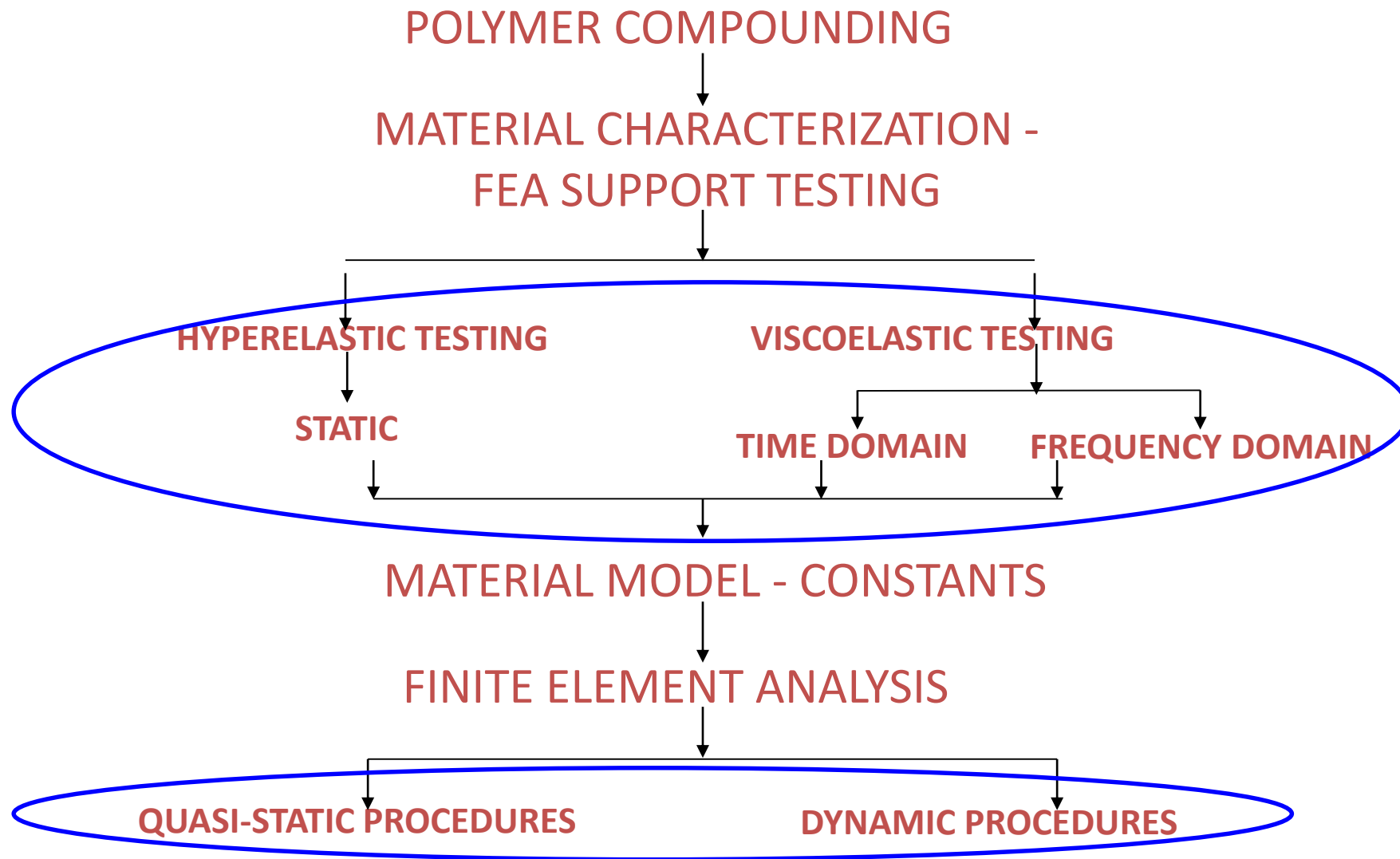
NABL ISO/IEC 17025:2017 ACCREDITED LAB



Accredited for;

- 1. Static Testing**
- 2. Dynamic Testing**
- 3. Fatigue Testing**

POLYMER ANALYSIS METHODOLOGY



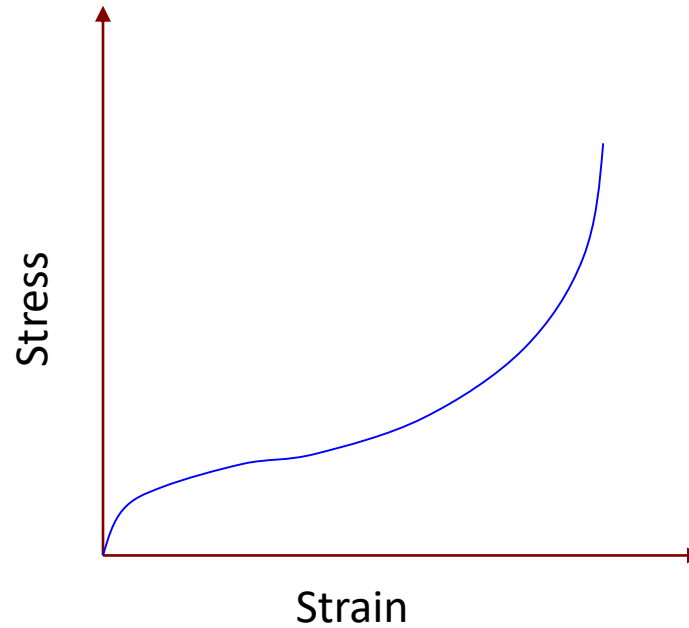
COMPLEXITIES IN THE FEA OF POLYMERS

- The Stress-Strain relationship is highly non-linear.
- Strain range can vary from 5 % to 700 %.
- Imperative to use large deflection theory.
- Stress-Strain characteristics are temperature dependent and hysteresis effects are significant.
- Rate effects are highly pronounced.
- Too many material models using different approaches.

MAJOR FEA CODES IN THE MARKET

- **Abaqus[®]** - Implicit and Explicit – Rubber
- **Ansys[®]** - Implicit – Rubber
- **Calculix** - Implicit and Explicit – Rubber
- **Comsol[®]** - Implicit– Rubber (50%)
- **LS-Dyna[®]** - Implicit and Explicit – Rubber
- **MSC Marc-Nastran[®]** - Implicit and Explicit – Rubber

HYPERELASTIC CONSTITUTIVE MODELS



Stretch Ratio (λ)

$$\lambda = 1 + \text{Strain} = 1 + \varepsilon$$

Input:

Stress-Strain Data from Main Deformation modes

$$W = \text{Constants}(I_1(\lambda), I_2(\lambda), I_3(\lambda))$$

$$W = C_{10}, C_{01}, \alpha_i, \mu_i (I_1(\lambda), I_2(\lambda), I_3(\lambda))$$

$$I_1 = \lambda_1^2 + \lambda_2^2 + \lambda_3^2$$

$$I_2 = \lambda_1^2 \lambda_2^2 + \lambda_2^2 \lambda_3^2 + \lambda_3^2 \lambda_1^2$$

$$I_3 = \lambda_1^2 \lambda_2^2 \lambda_3^2$$

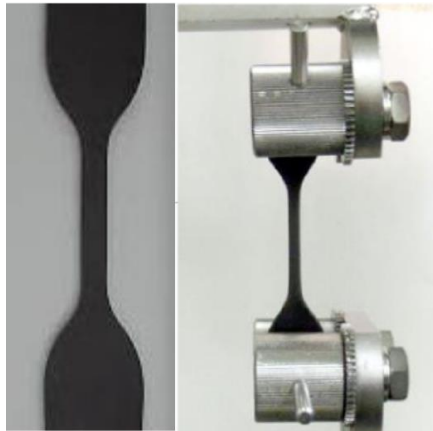
HYPERELASTIC MATERIAL CHARACTERIZATION TESTING

1. Five Deformation Modes

- **Uniaxial tension**
- **Uniaxial compression**
- **Planar shear**
- **Volumetric compression**
- **Equibiaxial tension**

2. Testing speed = quasi-static procedure

3. Minimum of 3 specimens



Uniaxial Tension Test

$$\lambda_1 = \lambda_T, \lambda_2 = \lambda_3 = \lambda_T^{-1/2}$$



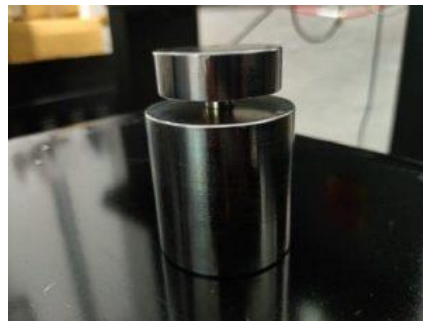
Uniaxial Compression Test

$$\lambda_1 = \lambda_C, \lambda_2 = \lambda_3 = \lambda_C^{-1/2}$$



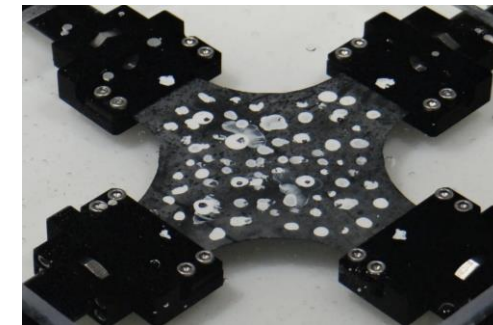
Planar Shear Test

$$\lambda_1 = \lambda_s, \lambda_2 = 1, \lambda_3 = \lambda_s^{-1}$$



Volumetric Compression Test

$$\lambda_1 = \lambda_2 = \lambda_3 = \lambda_v$$



Equibiaxial Tension Test

$$\lambda_1 = \lambda_2 = \lambda_B, \lambda_3 = 1/\lambda_B^2$$

STRESS AND STRAIN MEASURES

2nd Piola Kirchhoff stress – Cauchy's stress

Cauchy's stress = Force / Final area

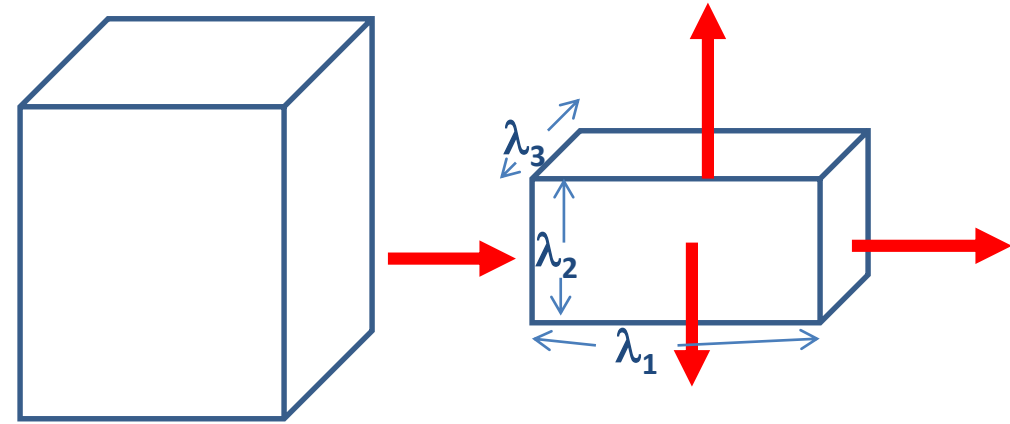
2nd Piola Kirchhoff stress = Force / Original area

Green Strain – True strain

True Strain = dL/L

Green Strain = dL/L + Nonlinear terms

The deformation
is described by
stretch ratios:
 $\lambda_1, \lambda_2, \lambda_3$

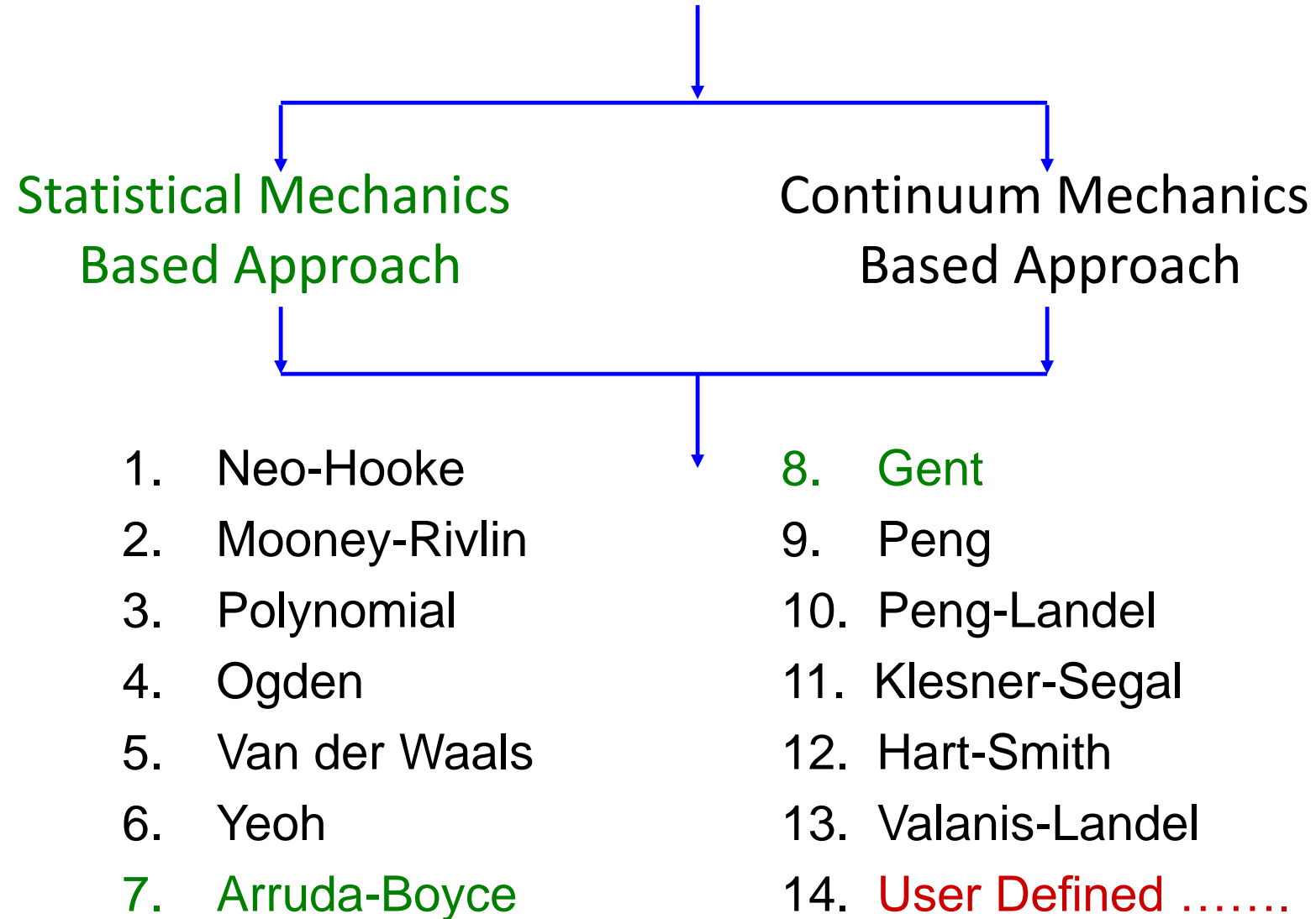


Strain Energy W

A simple relation for the strain energy density is:

$$W = (E/6) (\lambda_1^2 + \lambda_2^2 + \lambda_3^2 - 3) \quad \text{-----} \quad 1$$

MATERIAL MODELS



STRESS - STRAIN RELATIONS

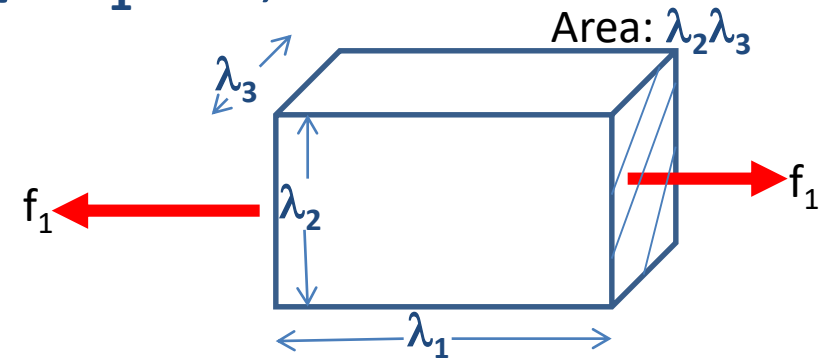
We can calculate stresses from the relation for **W**.

$\Delta W = f_1 d\lambda_1$. Hence: $\mathbf{t_1 = \lambda_1 \partial W / \partial \lambda_1 + P}$, etc.

where **P** is an
undetermined
hydrostatic
pressure

Note: we have assumed
incompressibility:

$$\lambda_1 \lambda_2 \lambda_3 = 1$$

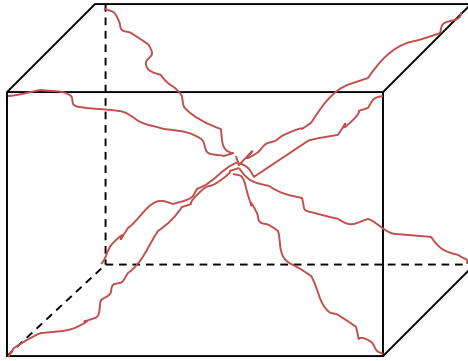


$$f_1 = t_1 \lambda_2 \lambda_3 \\ = t_1 / \lambda_1$$

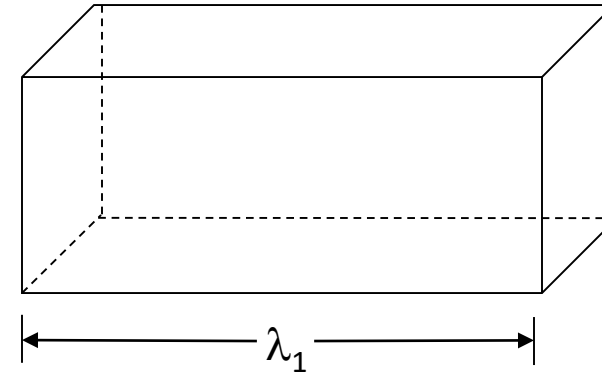
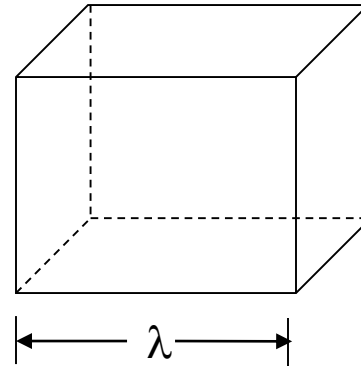
$$t_1 = \lambda_1 (\partial W / \partial \lambda_1) + p$$

$$t_2 = \lambda_2 (\partial W / \partial \lambda_2) + p$$

$$t_3 = \lambda_3 (\partial W / \partial \lambda_3) + p$$



8- Chain Network



Deformation in a Continuum Element

$$W(I_1, I_2, I_3) = \sum_{IJK=0}^N C_{ijk} (I_1 - 3)^i (I_2 - 3)^j (I_3 - 3)^k + \sum_{i=1}^N \frac{1}{D_i} (J^{el} - 1)^{2i}$$

Neo-Hookean Model: $W = C_{10}(I_1 - 3)$

Mooney-Rivlin Model: $W = C_{10}(I_1 - 3) + C_{01}(I_2 - 3)$

Ogden Model: $W = \sum_{i=1}^N \frac{2\mu_i}{\alpha_i^2} (\lambda_1^{-\alpha_i} + \lambda_2^{-\alpha_i} + \lambda_3^{-\alpha_i} - 3)$

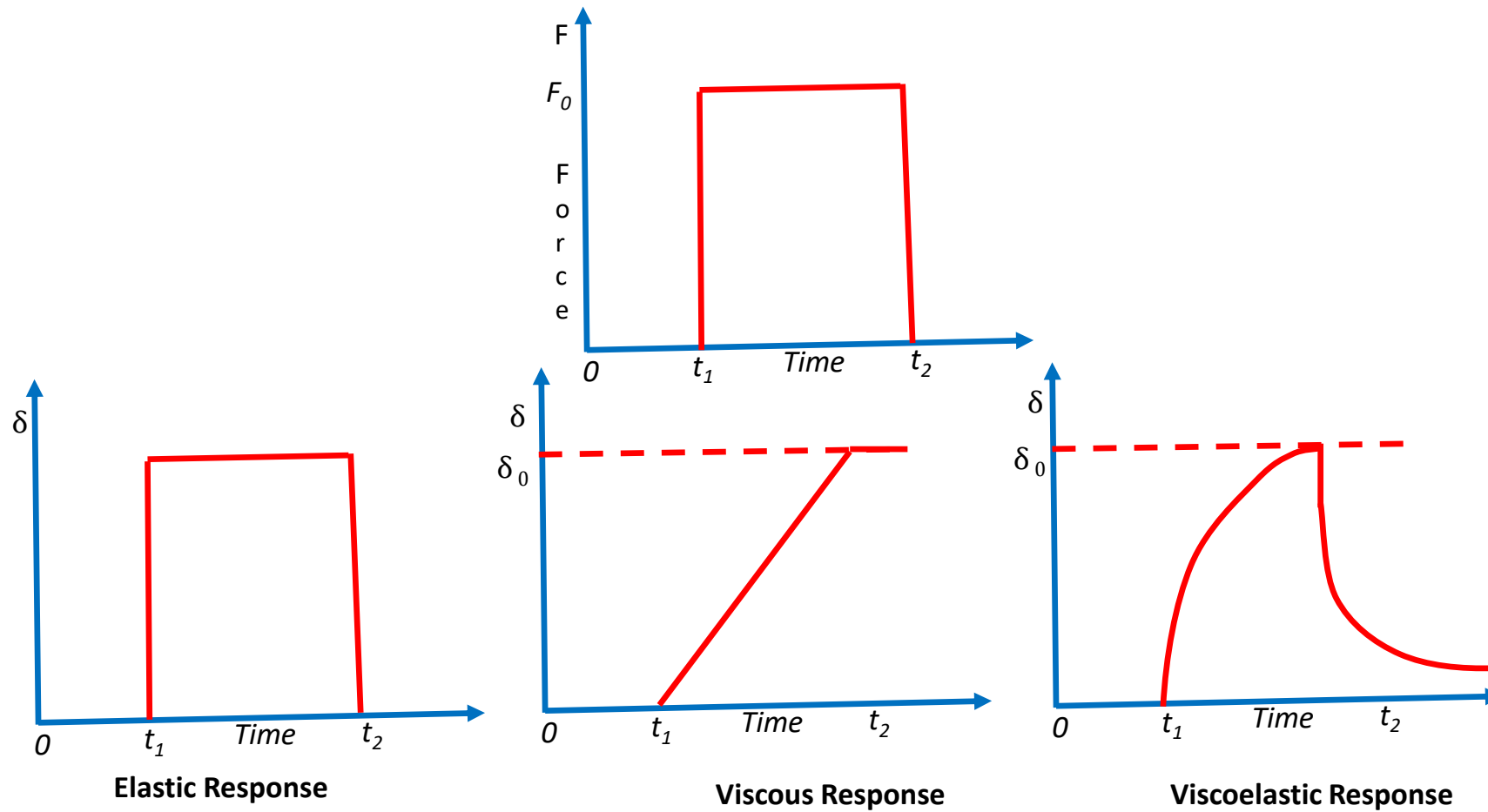
TIME DOMAIN VISCOELASTIC TESTING

- STRESS RELAXATION
- CREEP

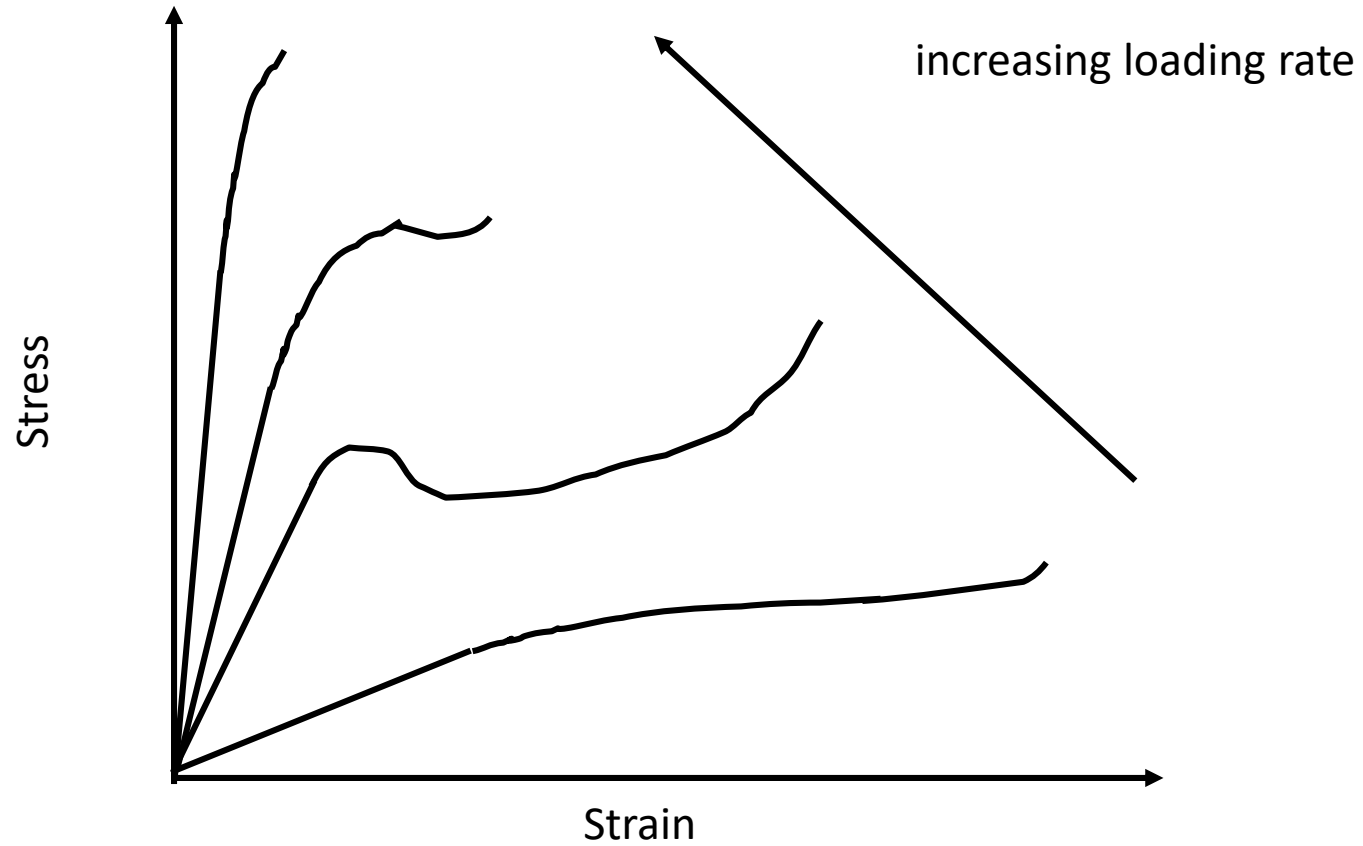
FREQUENCY DOMAIN VISCOELASTIC TESTING

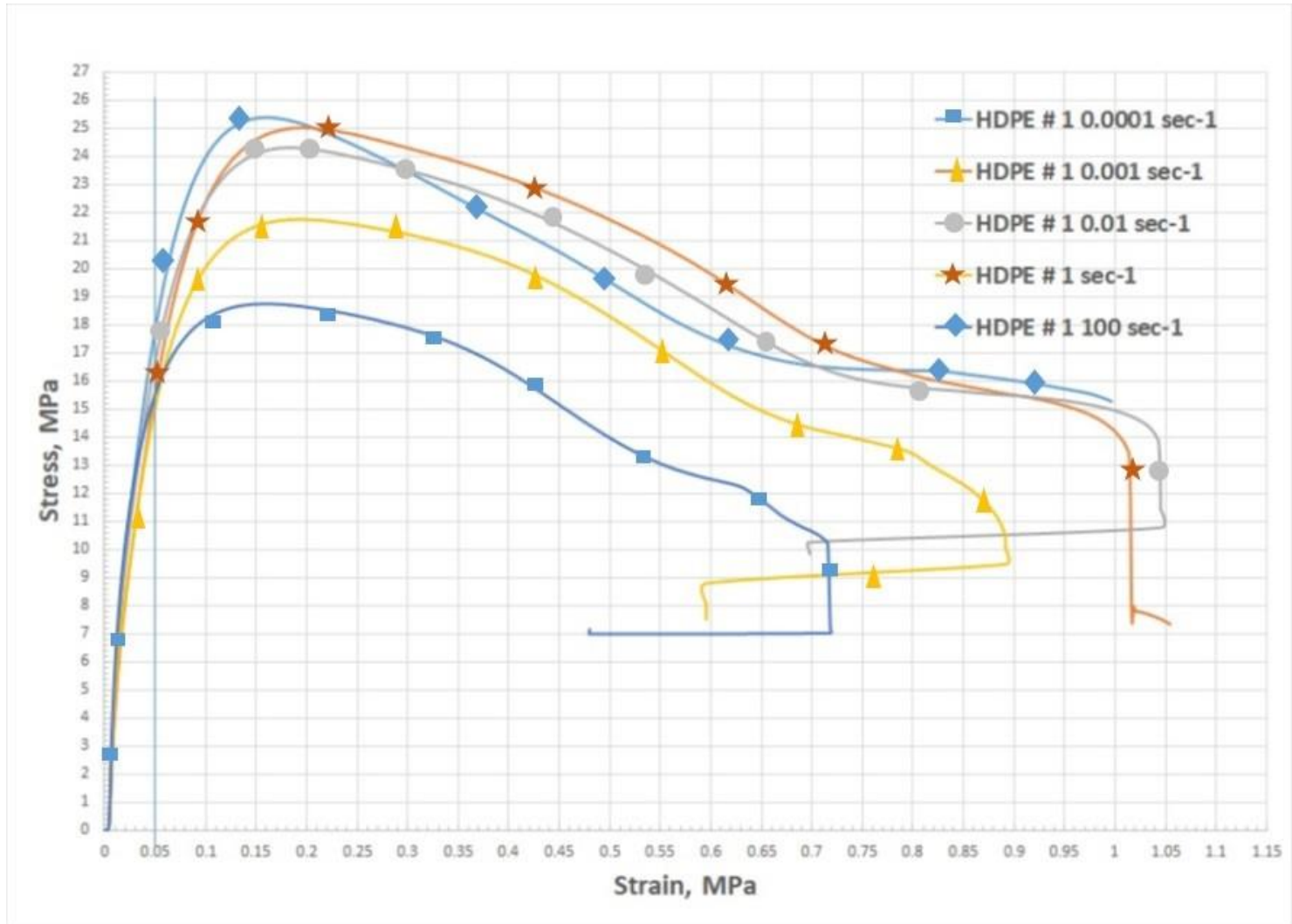
- STRAIN SWEEPS
- FREQUENCY SWEEPS

APPLIED LOAD AND RESULTANT DEFORMATION



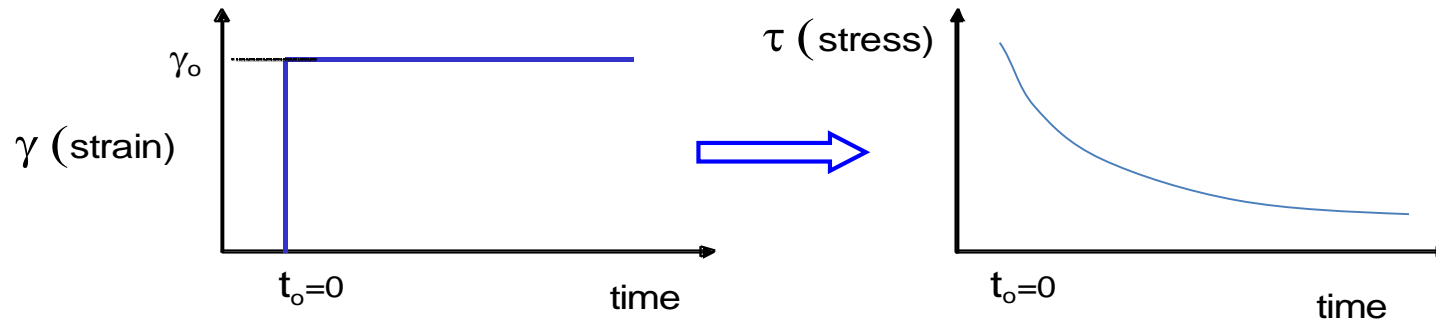
LOADING RATE VS. MODULUS





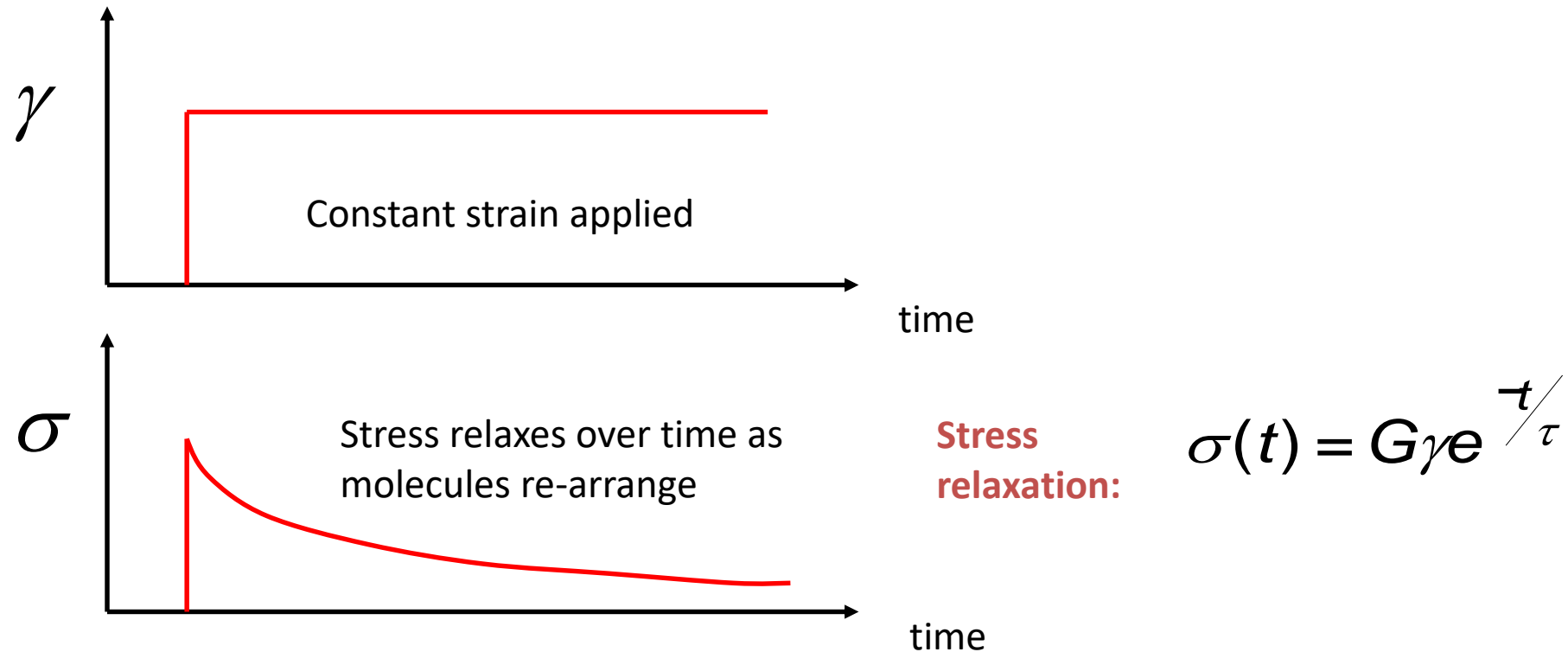
VISCOELASTICITY AND STRESS RELAXATION

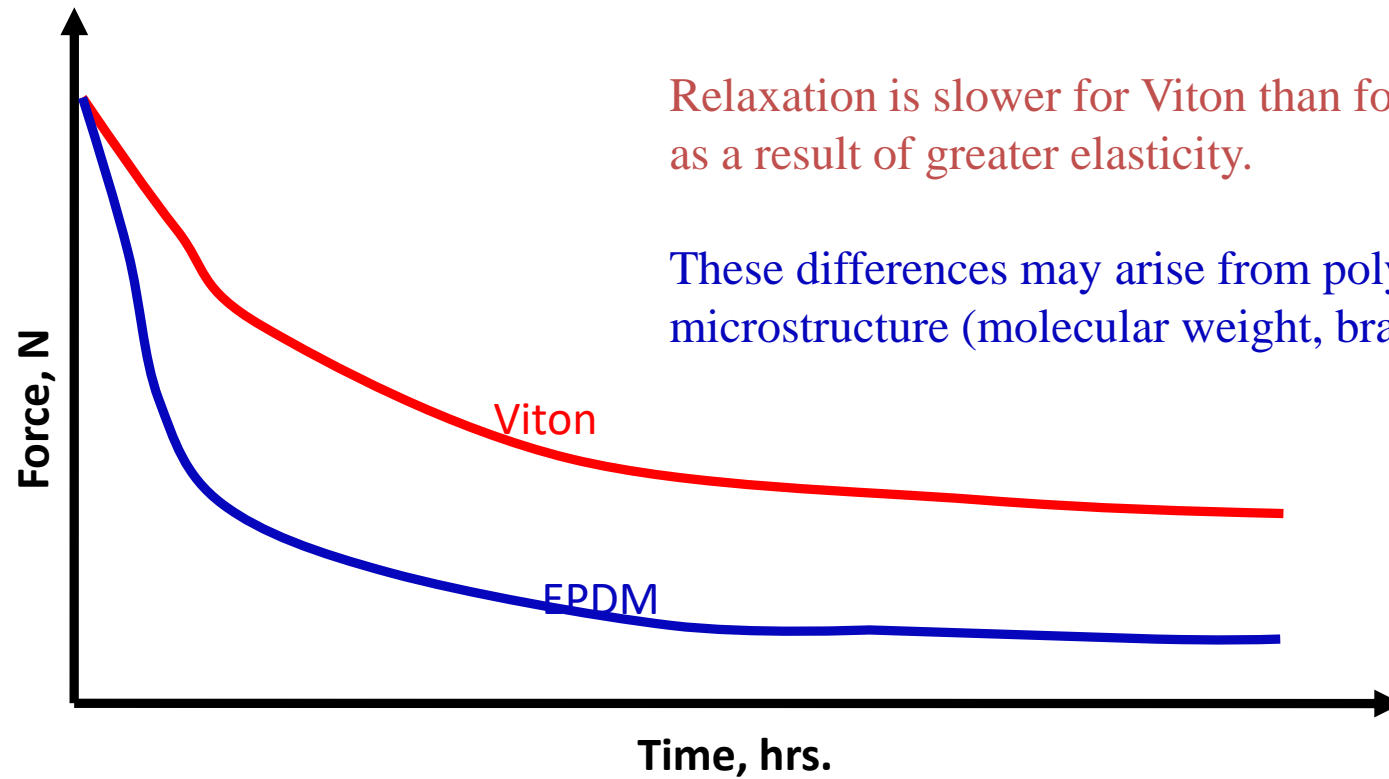
Whereas steady-shear measurements probe material responses under a steady-state condition, creep and stress relaxation monitor material responses as a function of time.



- Stress relaxation studies the effect of a step-change in strain on stress.

PHYSICAL MEANING OF THE RELAXATION TIME





Relaxation is slower for Viton than for EPDM, as a result of greater elasticity.

These differences may arise from polymer microstructure (molecular weight, branching).

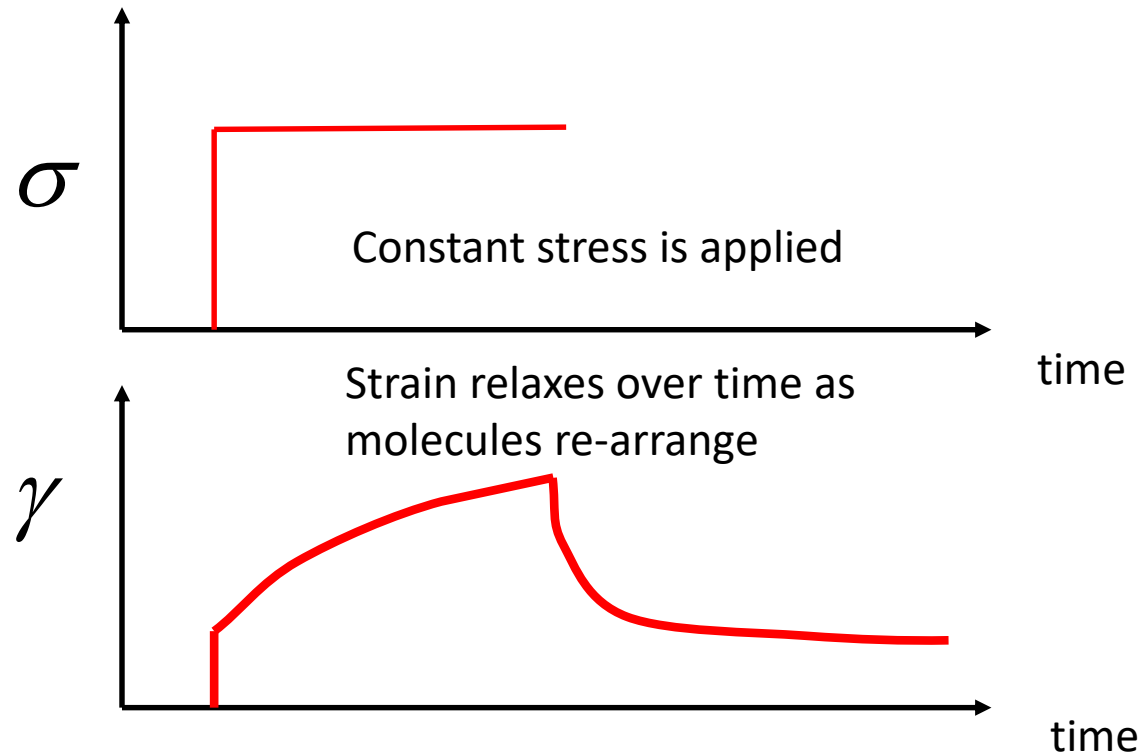
Viton

EPDM

Time, hrs.

Force, N

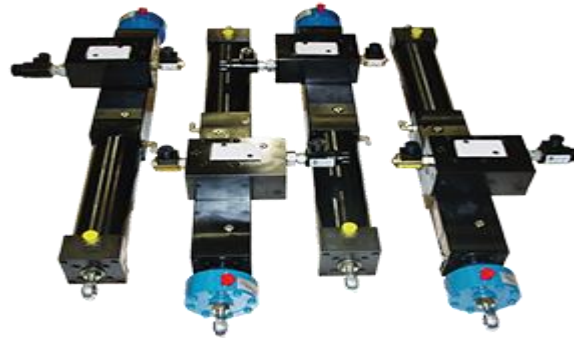
CREEP



Constant stress is applied and the strain relaxes as function of time

MATERIAL TESTING

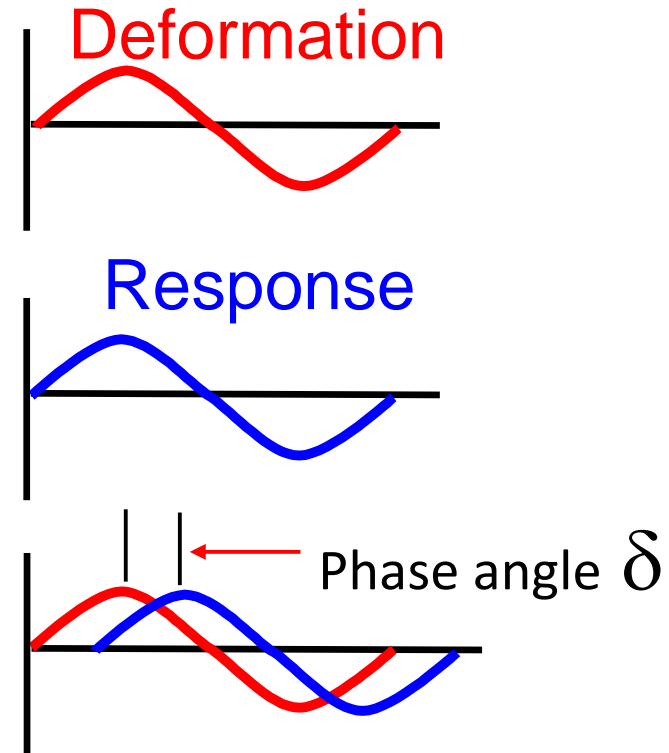
- MODULUS (STATIC/DYNAMIC)
- TAN δ
- CRACK GROWTH PROPAGATION



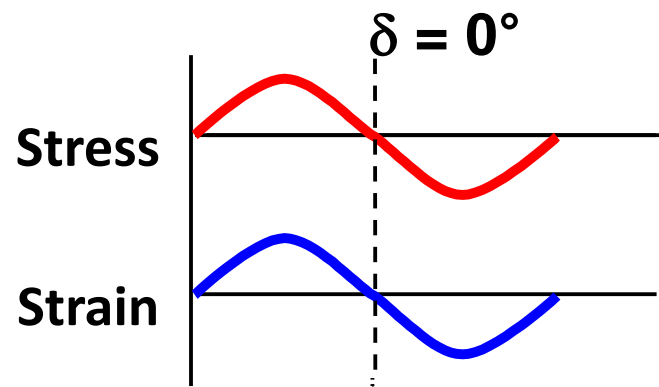
Courtesy: Dynamic Testing Equipments

DYNAMIC MECHANICAL TESTING

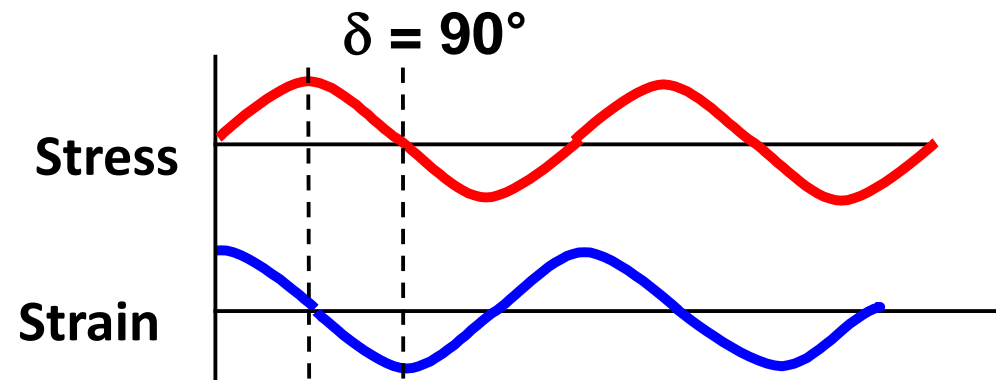
- An oscillatory (sinusoidal) deformation (stress or strain) is applied to a sample.
- The material response (strain or stress) is measured.
- The phase angle δ , or phase shift, between the deformation and response is measured.



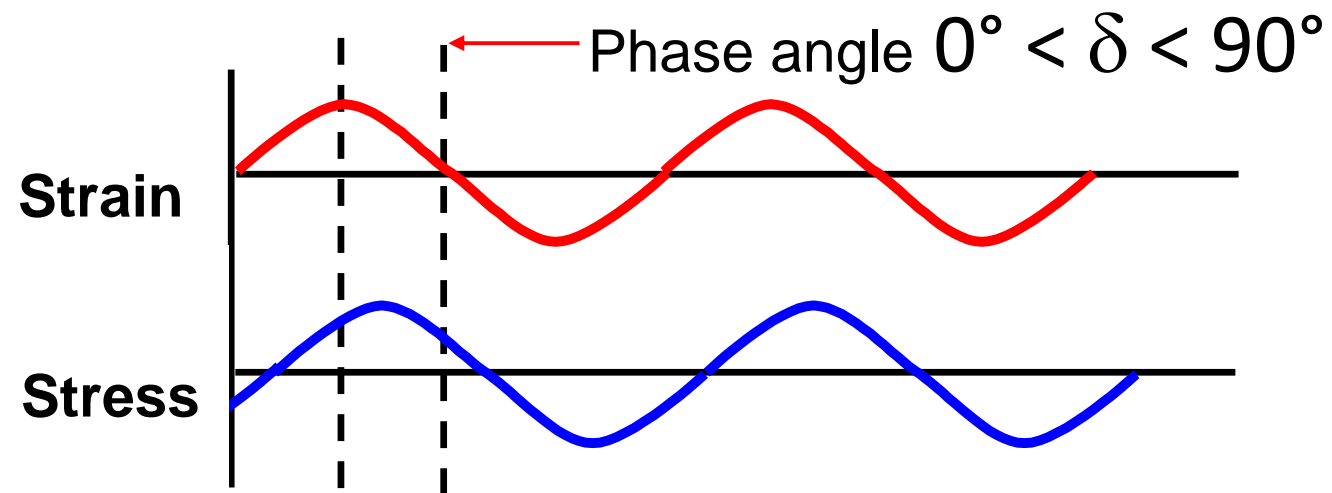
Purely Elastic Response (Hookean Solid)



Purely Viscous Response (Newtonian Liquid)

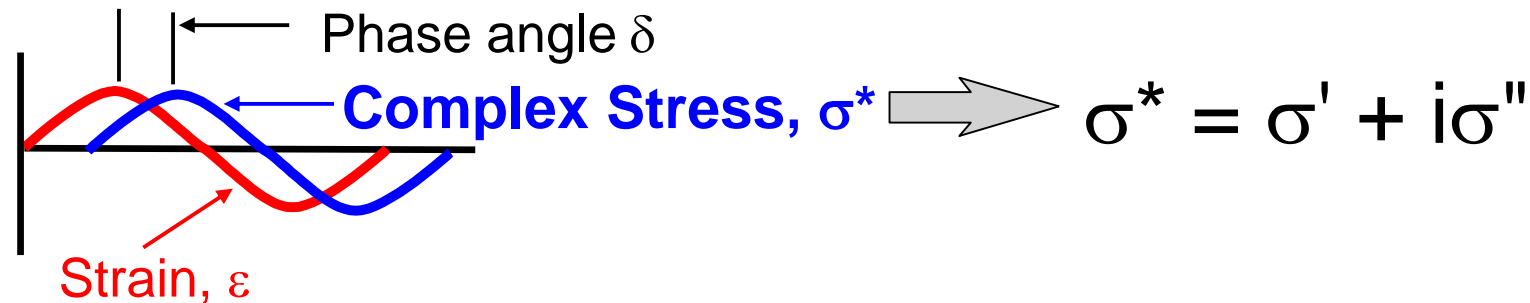


DYNAMIC MECHANICAL TESTING: VISCOELASTIC MATERIAL RESPONSE



Viscoelastic Parameters: The Complex, Elastic, & Viscous Stress

- The stress in a dynamic experiment is referred to as the complex stress σ^*
- The complex stress can be separated into two components:
 - 1) An elastic stress in phase with the strain. $\sigma' = \sigma^* \cos \delta$
 σ' is the degree to which material behaves like an elastic solid.
 - 2) A viscous stress in phase with the strain rate. $\sigma'' = \sigma^* \sin \delta$
 σ'' is the degree to which material behaves like an ideal liquid.



VISCOELASTIC PARAMETERS

The Modulus: Measure of materials overall resistance to deformation.

$$G = \text{Stress/Strain}$$

The Elastic (Storage) Modulus:
Measure of elasticity of material. The ability of the material to store energy.

$$G' = (\text{stress/strain})\cos\delta$$

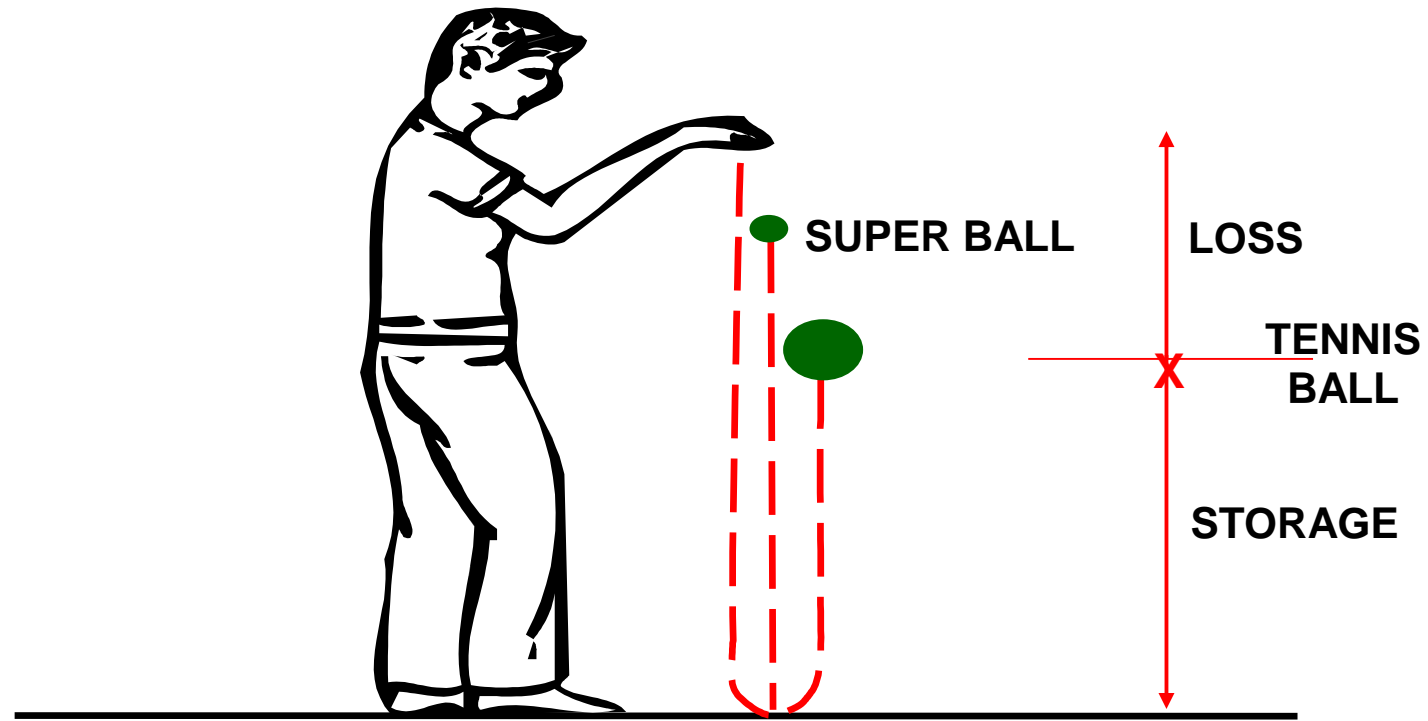
The Viscous (loss) Modulus:
The ability of the material to dissipate energy. Energy lost as heat.

$$G'' = (\text{stress/strain})\sin\delta$$

Tan Delta:
Measure of material damping - such as vibration or sound damping.

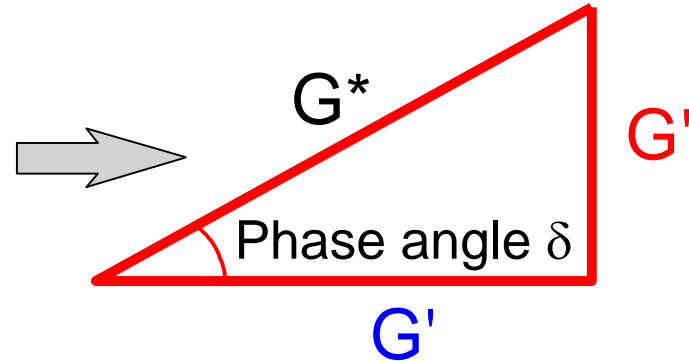
$$\tan \delta = G''/G'$$

STORAGE AND LOSS OF A VISCOELASTIC MATERIAL



VISCOELASTIC PARAMETERS: DAMPING, TAN δ

Dynamic measurement represented as a vector

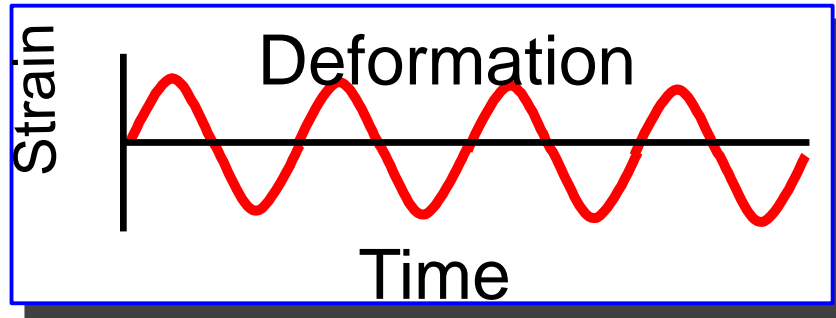


- The tangent of the phase angle is the ratio of the loss modulus to the storage modulus.

$$\tan \delta = G''/G'$$

- "TAN DELTA" ($\tan \delta$) is a measure of the damping ability of the material.

DYNAMIC TIME SWEEP



- The material response is monitored at a constant frequency, amplitude and temperature.

▲ INSTRUMENT MODE

Multi-Frequency

▲ METHOD

Equilibrate at ____ °C

Isotherm for ____ min.

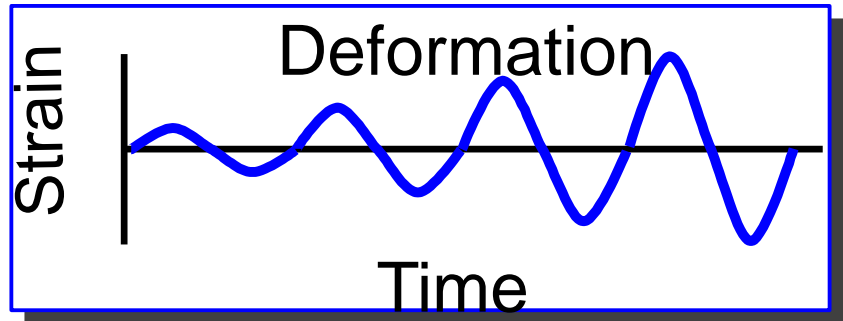
▲ **Frequency** = single/multiple

▲ **Amplitude** = In Linear viscoelastic region

• USES

- ↙ Cure Studies
- ↙ Degradation

DYNAMIC STRAIN SWEEP



- The material response to increasing deformation amplitude is monitored at a constant frequency and temperature.

- USES

- ↙ Identify Linear Viscoelastic Region
- ↙ Resilience

▲ INSTRUMENT MODE

Multi-Strain

▲ METHOD

Equilibrate at ____ °C

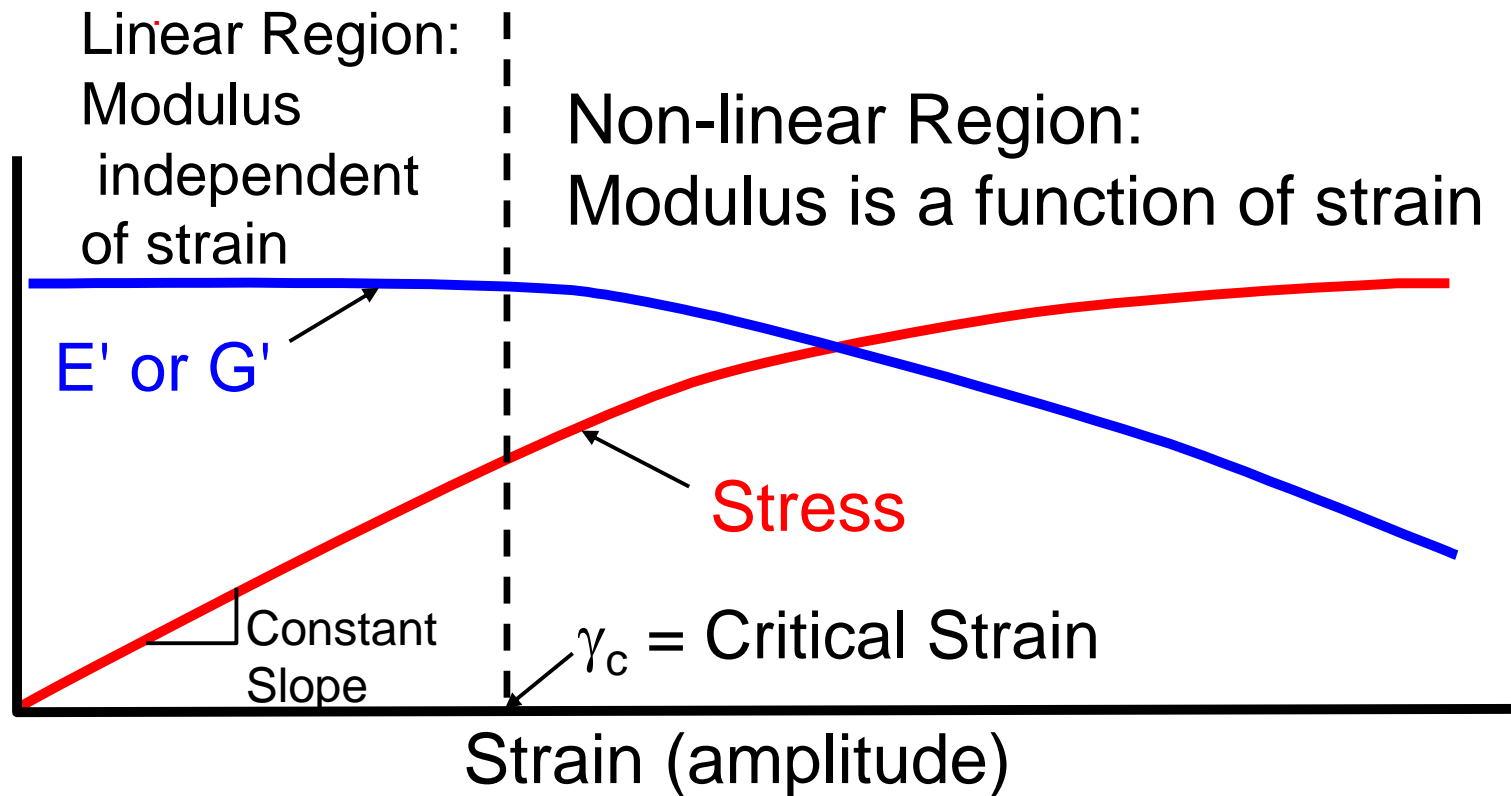
Isotherm for ____ min.

Strain Sweep

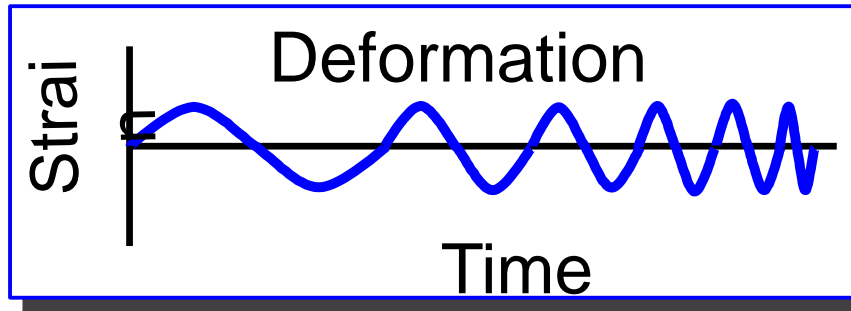
▲ Frequency = single only

▲ Amplitude = Program Table up to 28 values

DYNAMIC STRAIN SWEEP: MATERIAL RESPONSE



FREQUENCY SWEEP



▲ INSTRUMENT MODE

Multi-Frequency

▲ METHOD

Equilibrate at ____ °C

Isotherm for ____ min.

Frequency Sweep

▲ Frequency = Program Table up to 28 values

▲ Amplitude = single only In Linear viscoelastic region

- The material response to increasing frequency (rate of deformation) is monitored at a constant amplitude and temperature.

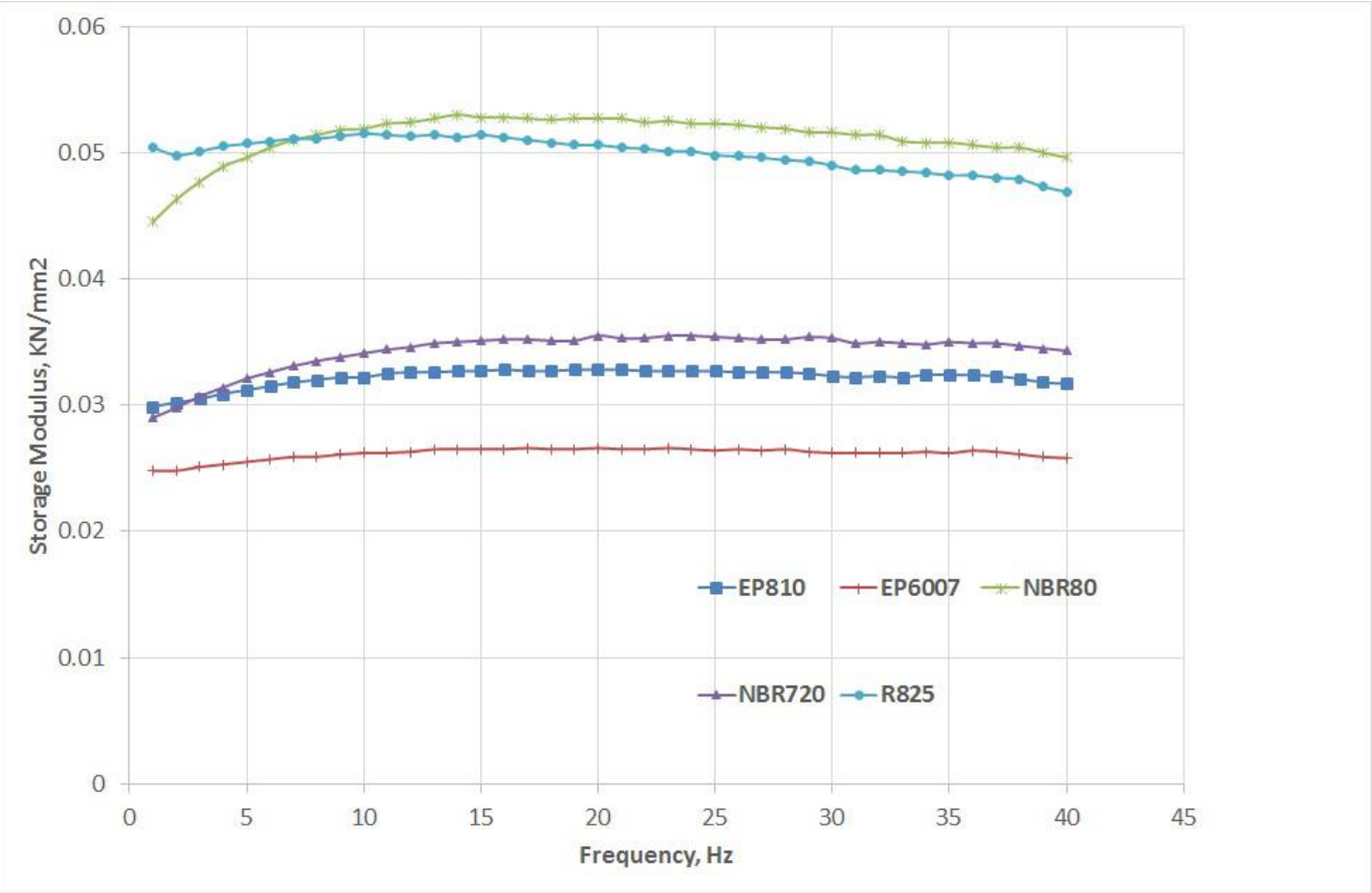
• USES

- ↙ High and Low Rate (short and long time) modulus properties.
- ↙ Polymer melt processing (shear sandwich).
- ↙ Extend range with TTS

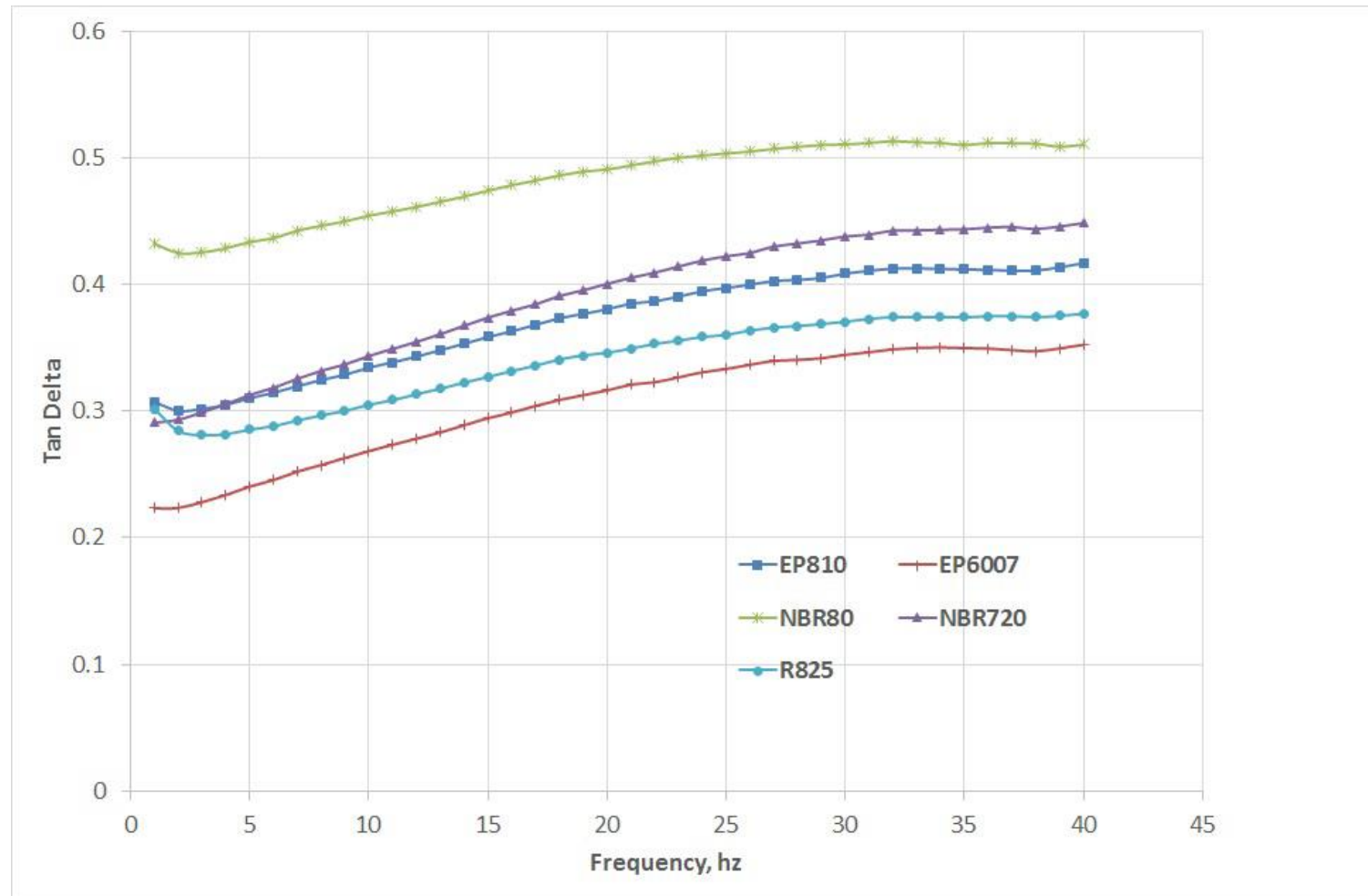
MATERIAL CHARACTERIZATION DMA TEST DATA

KS									
Step No.	Fundamental Frequency	Dynamic Stiffness	Damping	Delta	Phase	Complex Modulus	Storage Modulus	Loss Modulus	TanDelta
	Hz	kN/mm	kNs/mm	Degrees	rad	kN/mm^2	kN/mm^2	kN/mm^2	
1	1	1.66425	0.05775	14.09262	0.245963	0.04953	0.04836	0.010725	0.29016
2	2	1.66575	0.028875	14.1101	0.246268	0.04953	0.04836	0.010725	0.2912
3	3	1.685125	0.019875	14.38483	0.251063	0.050115	0.048945	0.011115	0.299
4	4	1.702	0.015375	14.73293	0.257138	0.0507	0.049335	0.011505	0.300875
5	5	1.717125	0.01275	15.13568	0.264168	0.05109	0.049725	0.011895	0.31239
6	6	1.7335	0.011	15.4504	0.26966	0.051675	0.050115	0.012285	0.31915
7	7	1.746125	0.00975	15.8461	0.276567	0.052065	0.050505	0.012675	0.32773
8	8	1.75425	0.00875	16.16373	0.28211	0.05226	0.050505	0.013065	0.33462
9	9	1.76575	0.008	16.49682	0.287924	0.05265	0.050895	0.013455	0.34177
10	10	1.773	0.007375	16.82195	0.293599	0.052845	0.05109	0.01365	0.34879
11	11	1.7815	0.00675	17.12603	0.298906	0.05304	0.05109	0.01404	0.35542
12	12	1.789375	0.006375	17.40917	0.303847	0.053235	0.051285	0.014235	0.36153
13	13	1.801625	0.006	17.70261	0.308969	0.053625	0.051675	0.014625	0.36803
14	14	1.805875	0.00575	18.03458	0.314763	0.05382	0.051675	0.01482	0.37531
15	15	1.812	0.005375	18.36453	0.320522	0.054015	0.051675	0.01521	0.38259
16	16	1.808875	0.005125	18.63523	0.325246	0.05382	0.051675	0.015405	0.38844
17	17	1.82025	0.005	18.93774	0.330526	0.05421	0.05187	0.015795	0.3952
18	18	1.812875	0.00475	19.21472	0.33536	0.054015	0.051675	0.01599	0.40131
19	19	1.820125	0.0045	19.43917	0.339278	0.05421	0.051675	0.016185	0.40625
20	20	1.824875	0.004375	19.66048	0.34314	0.054405	0.05187	0.01638	0.41119

PLOT OF STORAGE MODULUS VS FREQUENCY FROM A FREQUENCY SWEEP TEST



PLOT OF TAN DELTA VS FREQUENCY FROM A FREQUENCY SWEEP TEST



TIME DOMAIN AND FREQUENCY DOMAIN CALCULATIONS ON A DMA TEST DATA TO GENERATE VISCOELASTIC PROPERTIES

gi	ti	Frequency	Comp. Mod.	St. Mod.	Loss Mod.										Frequency			Prony series sum	
						Factor A	Factor B	Factor C	G-storage	G-loss	GI / Ginf	1-Gs/Ginf					time	relative modulus	
0	0.00001	1	0.0123	0.0121	0.0022	0.5	2.5000000E-01	7.1801780E-02	7.5000000E-01	7.1801780E-02	1.4360356E-01	-5.00000E-01	0	0	1	0	1		
0	0.0001	3.0417	0.0125	0.0123	0.0024		2.9869758E-01	6.4162397E-02	7.9869758E-01	6.4162397E-02	1.2832479E-01	-5.97395E-01	0	0	3.0417	0.00001	0.99989		
0	0.001	5.0833	0.0128	0.0125	0.0026		3.1702684E-01	6.6567664E-02	8.1702684E-01	6.6567664E-02	1.3313533E-01	-6.34054E-01	0	0	5.0833	0.0001	0.99889		
0.1	0.01	7.125	0.013	0.0127	0.0029		3.3222530E-01	6.9655339E-02	8.3222530E-01	6.9655339E-02	1.3931068E-01	-6.64451E-01	0	0	7.125	0.001	0.98938		
0.1	0.1	9.1667	0.0136	0.013	0.0031		3.4530574E-01	7.0882270E-02	8.4530574E-01	7.0882270E-02	1.4176454E-01	-6.90611E-01	0	0	9.1667	0.01	0.92617		
0.1	1	11.2083	0.01355	0.0131	0.0033		3.5612177E-01	7.0578545E-02	8.5612177E-01	7.0578545E-02	1.4115709E-01	-7.12244E-01	0	0	11.2083	0.1	0.82618		
0.1	10	13.25	0.0135	0.0131	0.0035		3.6486380E-01	6.9439429E-02	8.6486380E-01	6.9439429E-02	1.3887886E-01	-7.29728E-01	0	0	13.25	0.2	0.79323		
0.1	100	15.2917	0.0136	0.0131	0.0037		3.7189996E-01	6.7979272E-02	8.7189996E-01	6.7979272E-02	1.3595854E-01	-7.43800E-01	0	0	15.2917	0.3	0.77581		
0	1000	17.3333	0.0137	0.0132	0.0039		3.7760938E-01	6.6497703E-02	8.7760938E-01	6.6497703E-02	1.3299541E-01	-7.55219E-01	0	0	17.3333	0.4	0.76454		
0	10000	19.375	0.014	0.0134	0.0041		3.8231438E-01	6.5145259E-02	8.8231438E-01	6.5145259E-02	1.3029052E-01	-7.64629E-01	0	0	19.375	0.5	0.75595		
		21.4167	0.0141	0.0134	0.0042		3.8626635E-01	6.3984961E-02	8.8626635E-01	6.3984961E-02	1.2796992E-01	-7.72533E-01	0	0	21.4167	0.6	0.74871		
0.5		23.4583	0.0141	0.01345	0.0042		3.8965495E-01	6.3032297E-02	8.8965495E-01	6.3032297E-02	1.2606459E-01	-7.79310E-01	0	0	23.4583	0.7	0.74229		
		25.5	0.0142	0.0135	0.0044		3.9262150E-01	6.2278684E-02	8.9262150E-01	6.2278684E-02	1.2455737E-01	-7.85243E-01	0	0	25.5	0.8	0.73648		

G_0=1

G_inf=0.5

Normalized Modulus Vs. Frequency

— Storage Modulus
— Loss Modulus

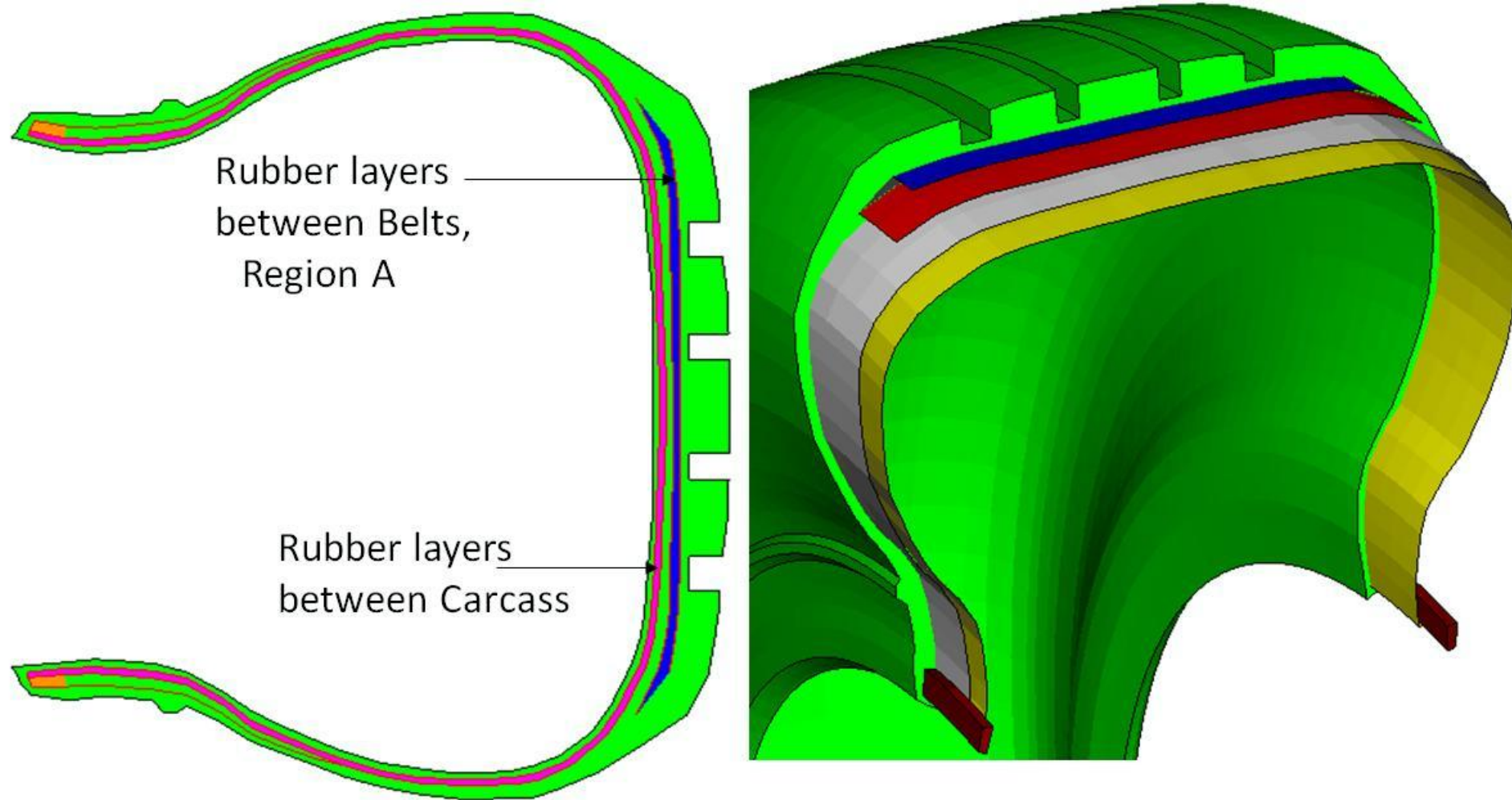
Stress Relaxation Vs. Time

$$G'(\omega) = \underbrace{G_0 \left(1 - \sum_{i=1}^N g_i^P \right)}_{\text{Factor A}} + \underbrace{G_0 \sum_{i=1}^N \frac{g_i^P \tau_i^2 \omega^2}{1 + G \tau_i^2 \omega^2}}_{\text{Factor B}}$$
$$G''(\omega) = \underbrace{G_0 \sum_{i=1}^N \frac{g_i^P \tau_i \omega}{1 + \tau_i^2 \omega^2}}_{\text{Factor C}}$$

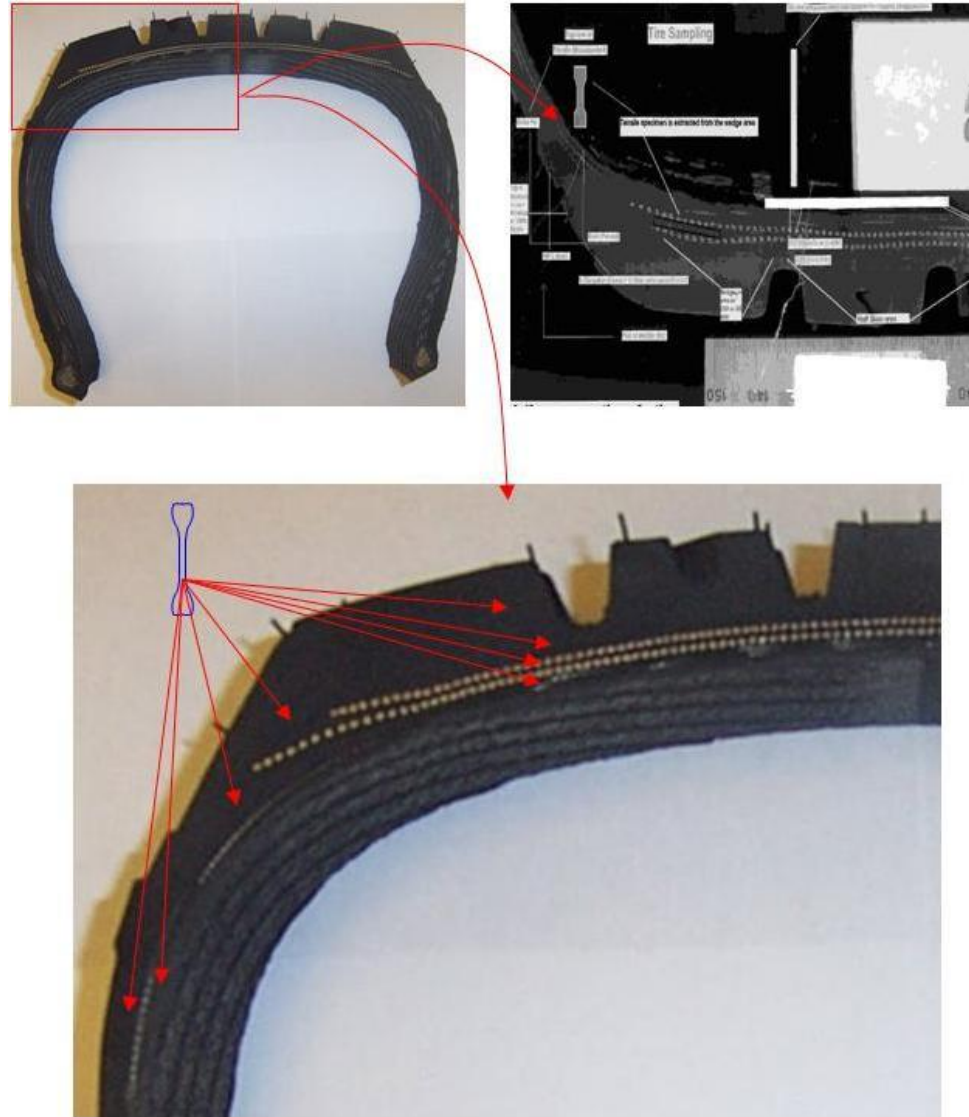
$$G'(\omega) = \underbrace{G_0 \left(1 - \sum_{i=1}^N g_i^P \right)}_{\text{Factor A}} + \underbrace{G_0 \sum_{i=1}^N \frac{g_i^P \tau_i^2 \omega^2}{1 + G \tau_i^2 \omega^2}}_{\text{Factor B}}$$

$$G''(\omega) = G_0 \underbrace{\sum_{i=1}^N \frac{g_i^P \tau_i \omega}{1 + \tau_i^2 \omega^2}}_{\text{Factor C}}$$

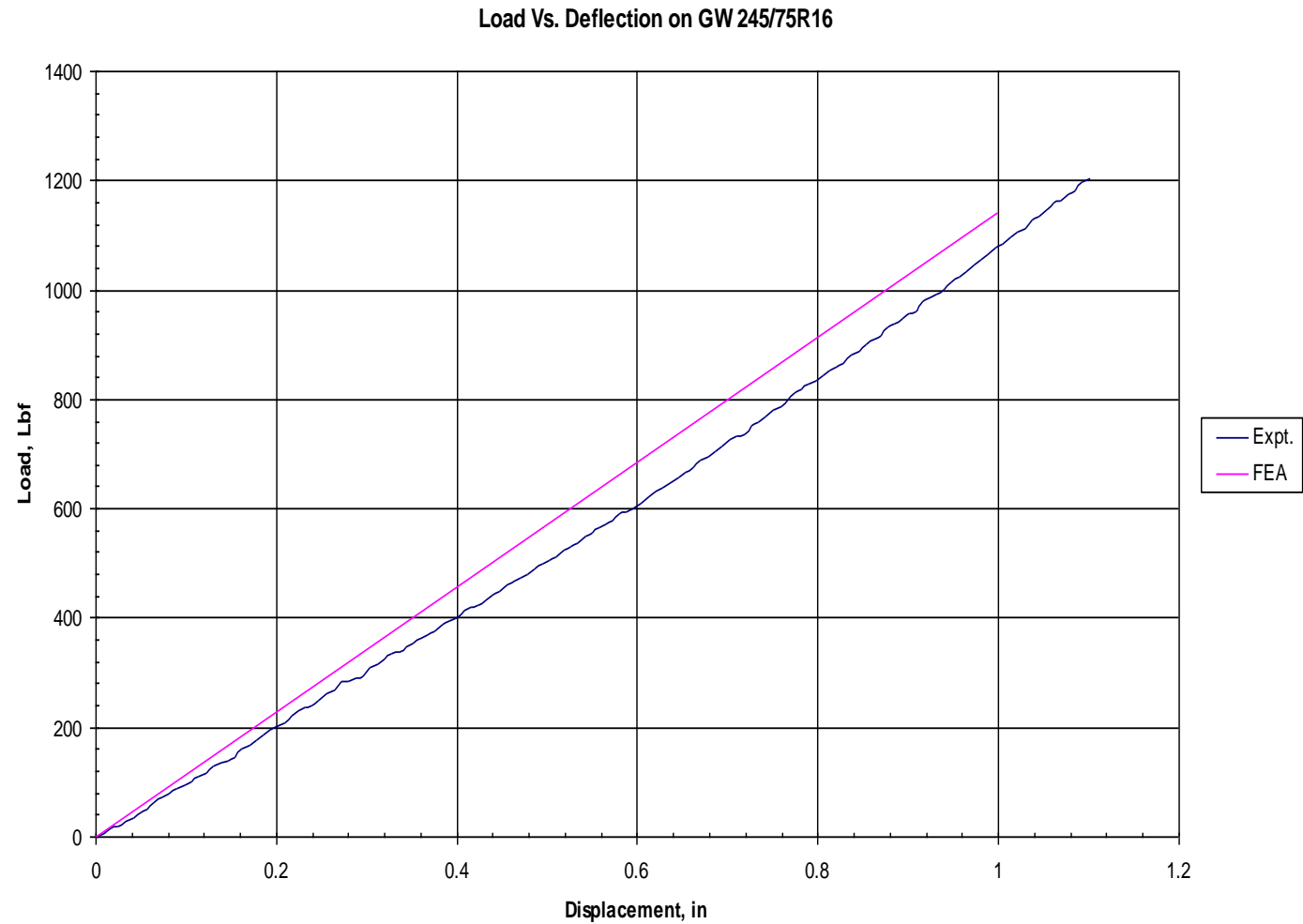
APPLICATION OF HYPERELASTIC & VISCOELASTIC DATA FOR TIRE PERFORMANCE ANALYSIS



MATERIAL EXTRACTION FOR TIRE FEA

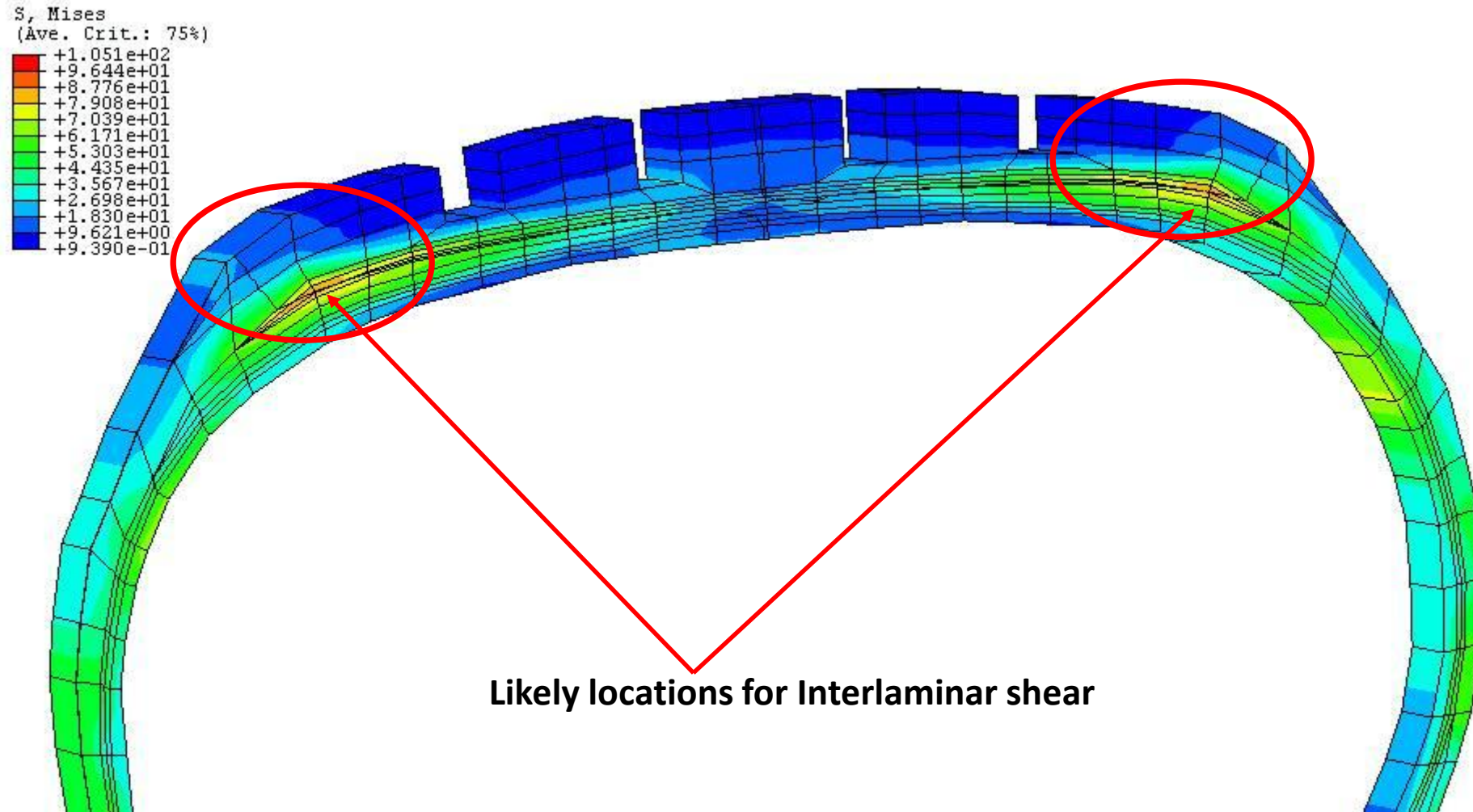


LOAD-DEFLECTION RESULTS



Comparison of Experimental and FEA Results

HYPERELASTIC TIRE ANALYSIS RESULTS

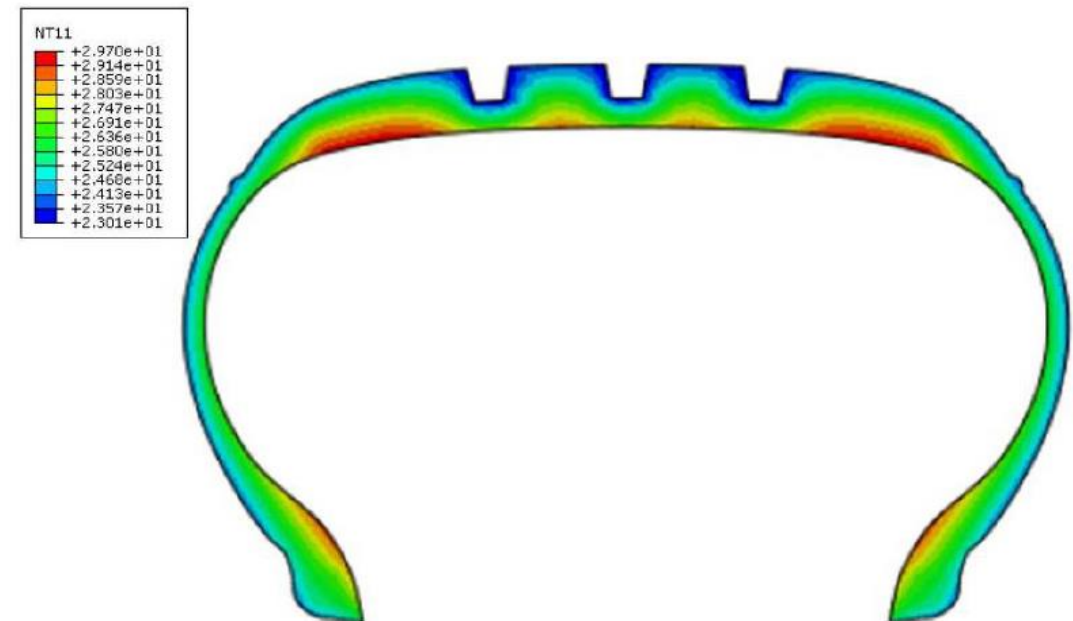


VISCOELASTIC TIRE ANALYSIS RESULTS FOR TEMPERATURE PREDICTION

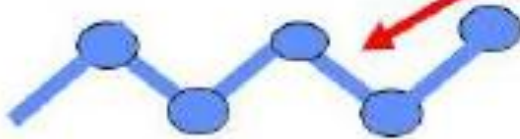
Non-linear Viscoelastic tire simulation is carried out using Abaqus/Ansys/Marc etc., to predict the hysteresis losses, temperature distribution and rolling resistance of a tire. The simulation includes several steps like (a) FE tire model generation, (b) Material parameter identification, (c) Material modeling and (d) Tire Rolling Simulation.

The energy dissipation and rolling resistance are evaluated by using dynamic mechanical properties like storage and loss modulus, tan delta etc. The heat dissipation energy is calculated by taking the product of elastic strain energy and the loss tangent of materials.

Tire Temperature Prediction during Rolling



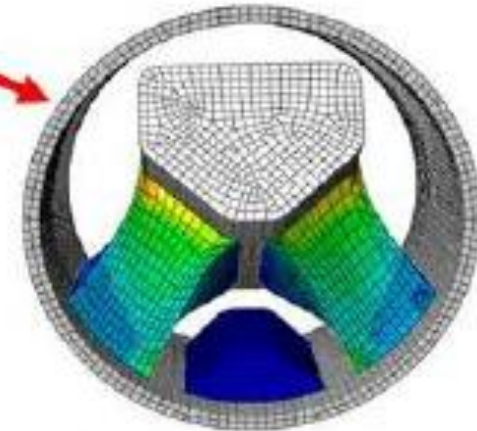
Dynamic Mechanical Testing Helps you Relate



Molecular Structure
Of Polymers



Manufacturing/
Material Processing



Mechanical Characteristics
And Performance

VERIFICATIONS AND VALIDATIONS

- Single Element Tests
 - Can be performed by analyst (uses curve-fitting)
 - First order check on the material property
- Closed Loop Validation
 - Compare results with the original material data from experiments
- Open Loop Validation
 - Comparison to alternate experimental modes
 - Carry out tests at component level

APPLICATION AREAS IN FEA

- Engine mounts, bushings, vibration isolators etc.
- Seals, o-rings etc.,
- Gaskets(Rubber and Composite)
- Weather strips
- Biomedical implants
- All situations where static pre-load is superimposed by service loads.

GOAL OF CAE TESTING SERVICES

- Create a step-by-step process based procedure for CAE.
- Validate for different regimes of product performance and service conditions
 - Viscoelastic
 - Hyperelastic
 - Hyperelastic rate dependent
 - Non-linear (Elasto-plastic, high strain rate)
- Validate models for failure analysis and design optimization

HOW CAN FEA HELP THE DESIGN ENGINEER & POLYMER TECHNOLOGIST

- Provides virtual testing and approaches to simulating complex material characteristics.
- use of FEA will reduce testing and redesign costs thereby shortening the product development time.
- Identify issues in designs before mold is made.
- Redesign components and systems before dependencies to other parts/components prohibit changes.
- Optimize design before prototyping.

EXPERIENCE BASED CONSULTING IN PRODUCT DEVELOPMENT AND MATERIAL TESTING

- Material Evaluation
- Product Design and Analysis
- Material Characterization and Durability Testing
- Failure Analysis
- Patent Development
- Feedback and Optimization of Rubber Compounds

PUBLICATIONS & REFERENCES

Srinivas, K., *Material Characterization And CAE For Non-Metallic Materials & Manufacturing Processes*, SAE Symposium on CAE Applications for Automotive Structures, Detroit, November 2005.

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Cornelius, K. C., and Srinivas, K., *Isentropic Compressible Flow for Non-Ideal Gas Model for a Venturi*, ASME Journal of Fluids Engineering, Feb 2004.

Srinivas, K., and Pannikottu, A., *Material Characterization and Finite Element Analysis of High Performance Tires*, International Rubber Expo and Conference, Mumbai, March 2005.

Srinivas, K., and Dharaiya, D., *Material And Rheological Characterization For Rapid Prototyping Of Elastomers Components*, American Chemical Society, Rubber Division, 170th Technical Meeting, Cincinnati, October 2006